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**IN THE SPECIFICATION**

\* NOTE: Reference to paragraph numbers in this section is with respect to the corresponding published U.S. Application 20060211342.

Please amend paragraph #0001 as follows:

"This application is a continuation-in-part of U.S. Ser. No. 10/120,969, filed April 11, 2002 (now U.S. Patent No. 6,679,758), and a ~~continuation-in-part~~ continuation-in-part of U.S. Ser. No. 10/328,802, filed December 24, 2002 (now U.S. Patent No. 6,988,937). The entire contents of U.S. Ser. No. 10/120,969 and U.S. Ser. No. 10/328,802 are hereby incorporated by reference."

Please amend paragraph #0032 as follows:

"The invention further includes bonded abrasive tools comprising a three-dimensional composite of (a) 22-46 vol % abrasive grains bonded with 4-20 vol % inorganic bond material; and (b) 40-68 vol % interconnected porosity; wherein a majority of the abrasive grains are present as irregularly spaced clusters within the composite; the bonded abrasive tools have elastic modulus values that are at least 10 % lower than elastic modulus values for otherwise identical ~~conventional~~ tools having regularly spaced abrasive grains within a three-dimensional composite; and the bonded abrasive tools exhibit a minimum burst speed of 4000 sfpm (20.32 m/s)."

Please amend paragraph #0039 as follows:

"(a) providing a bonded abrasive wheel comprising a three-dimensional composite of (i) 22-46 vol % abrasive grains bonded with 4-20 vol % inorganic bond material; and (ii) 40-68 vol % interconnected porosity; and wherein a majority of the abrasive grains are present as irregularly spaced clusters within the composite; the bonded abrasive tool has an elastic modulus value that is at least 10 % lower than the elastic modulus value of an otherwise identical ~~conventional~~ tool having regularly spaced abrasive grains within a three-dimensional composite; and the bonded abrasive tool has a minimum burst speed of 4000 sfpm (20.32 m/s)."

Please amend paragraph #0161 as follows:

"Wheel vibration during grinding was measured with IRD Mechanalysis equipment (Analyzer Model 855 Analyzer/Balancer, obtained from Entek Corporation,

North Westerville, Ohio). In an initial grinding run, vibration levels at various frequencies (as velocity in inches/second units) were recorded, using a fast ~~fourier~~-Fourier transform (FFT) procedure, at two and eight minutes after dressing the wheel. After the initial grinding run, a second grinding run was made and time-related growth in vibration level was recorded at a selected, target frequency (57000 cpm, the frequency observed during the initial run) during the entire 10.7 minutes the wheel remained in contact with the workpiece. Wheel wear rates (WWR), material removal rates (MRR) and other grinding variables were recorded as the grinding runs were made. These data, together with the vibration amplitude for each wheel after 9-10 minutes of continuous contact grinding, are shown in Table 3-1, below."

Please amend paragraph #0220 as follows:

"As can be seen from the grinding test results in Table 6-3, the experimental wheels exhibited higher MRR (10 to 68%) before failure ~~occured~~occurred, relative to comparative wheels having identical volume % compositions. At identical compositions, experimental wheels exhibited a reduction in power (3 to 31%) needed to grind (specific grinding energy). These grinding operation efficiencies were achieved without any significant loss of surface quality of the workpiece being ground. The ~~result~~-results suggest the experimental wheels could be operated in commercial creep feed grinding operations at a lower dressing rate with a constant MRR thereby achieving at least a doubling of wheel life."